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鄂尔多斯盆地延川南区块深部地应力状态 及其对煤层气开发效果的影响

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提要:延川南区块煤储层埋深在700~1500 m,多数深于900 m。基于该区块压裂施工压降数据,计算最大、最小水平主应力和垂向应力,划分储层地应力类型,分析了地应力及其类型对渗透率和压裂效果的影响。结果表明,研究区整体处于拉张状态,最大、最小水平主应力和垂向应力与埋深呈正相关线性关系。地应力类型以Ia类为主,III类其次,II类最少。Ia类地应力储层以垂直裂缝为主,裂缝指数最低,但应力敏感性弱,应力敏感性系数仅为0.479,且压裂缝半长最短,产气量最低,产水量最高。II类地应力储层主次裂缝宽分别为16 μm和11 μm,宽度最大,但储层应力敏感性最强。压裂以水平裂缝为主,裂缝指数最高,且压裂缝最长,改造效果最好,产气量最高。III类地应力储层裂缝复杂,渗透性和应力敏感性居中,压裂缝长居中,但产量相对较低,不能实现效益开发。

关 键 词:深部煤层;煤层气;地应力;压裂效果;渗透率;油气地质调查工程;延川区块;鄂尔多斯盆地

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Stress state of deep seam and its influence on development performance of CBM wells in South Yanchuan Block, Odors Basin

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Abstract: The buried depth of the coal seams of South Yanchuan block is between 700 m and 1500 m. And for the most area, the depth is deeper than 900 m. In order to clarify the in-situ stress state of deep coal-bed methane reservoir and its influence on the development of CBM wells, the maximum and minimum horizontal principal stress and the vertical stress are calculated based on the pressure drop data of hydraulic fracturing. The results show that the whole area is in the state of tension. The maximum horizontal principal stress, the minimum horizontal principal stress and the vertical stress are positively correlated with the buried depth. The type of the ground stress is mainly type Ia, followed by III type and II type. The reservoir with type Ia ground stress is dominated by vertical fractures with the lowest fracture index. However, the stress sensitivity is weak, and the stress sensitivity coefficient is only 0.479. The main and secondary fractures of type I stress reservoir are 16 μm and 11 μm respectively, with the

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largest width and the strongest reservoir stress sensitivity. Type I fractures are mainly horizontal fractures, with the highest fracture index, the longest compression fracture, the best reconstruction effect and the highest gas production. Reservoirs with type III in-situ stress develop complex fractures, with medium permeability, stress sensitivity and hydraulic fracture length. However, the production for type III is relatively low, and cannot achieve economic development.

Keywords: deep coal seam; coalbed methane; in-situ ground stress; fracturing performance; permeability; influence; oil-gas geological survey engineering; Yanchuan Block; Odors Bsain

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1 引言

深部煤层气是中国煤层气产业规模发展的基础,深部不代表具体的深度而是表征应力状态、含气量等发生了明显转折的深度,不同区块具有不同的具体深度(秦勇等,2016)。聂志宏等(2018)对大宁—吉县深部煤层气进行了研究,认为具有长期低产、上产缓慢和排采期更长的生产特征,其中应力状态对渗透率和储层改造效果的影响是主要因素(吴双等,2015)。因此,对深部煤储层应力状态特征进行研究具有重要意义。许多学者对不同区域的地应力状态进行了研究,徐宏杰等(2014)研究了黔西地区埋深及地应力对储层渗透率的控制,李勇等(2017)对鄂尔多斯盆地东缘的地应力状态及其影响进行了研究,刘洪林等(2007)对

沁水盆地南部埋深800m以浅的储层地应力进行了研究,杨延辉等(2015)对沁南—夏店区块,刘大锰等(2017)、李叶朋等(2017)就郑庄区块地应力对储层渗透率的影响进行了研究,但对不同地应力类型对天然裂缝形态影响研究较少。陈峥嵘等(2018)对沁水盆地地应力类型对压裂裂缝效果进行了研究,但埋深在700~800 m,埋深分布范围较小。延川南煤层气田位于鄂尔多斯盆地东南缘,位于晋西挠褶带和渭北隆起交界处(图1),整体为一倾向北西的单斜构造(陈贞龙等,2019)。研究区中部发育西掌断裂带,东部和西部分别为谭坪、万宝山构造带(付玉通等,2017),埋深由西向东增加,平均埋深在1250 m左右。2号煤层煤层垂直应力总体上大于最大水平主应力,整体处于拉张应力区(陈贞龙等,2018)。目前对不同地应力类型对天然裂缝形态影

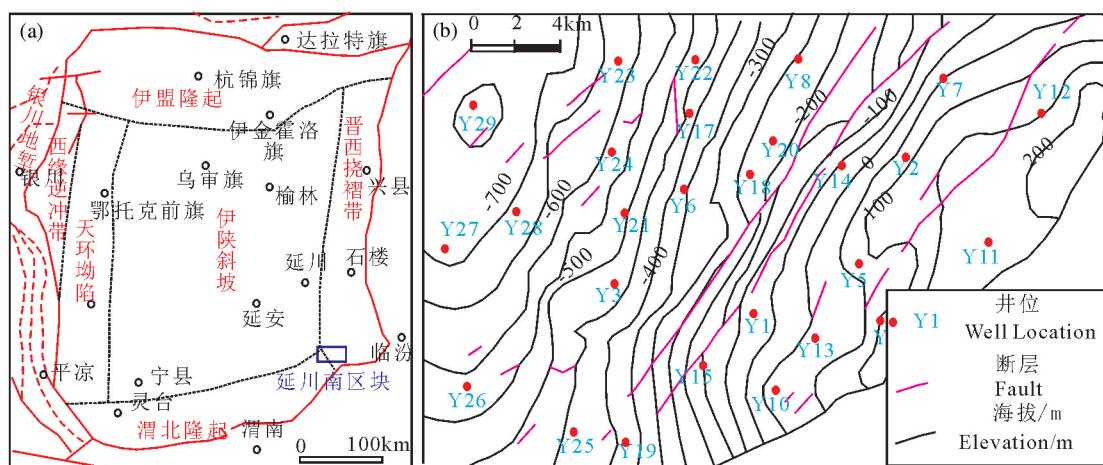


图1 延川南地理位置及地质构造图
a—延川南地理位置图;b—延川南地质构造图

Fig.1 Geological map showing structural location of South Yanchuan Block
a—Location of Yanchuan Nan Block;b—Structure of South Yanchuan Block

响以及延川南区块深部煤储层地应力状态的研究较少。本文围绕这两个问题,开展理论和实验分析,期望明确深部煤储层地应力状态及其对煤层气开发效果的影响。

2 地应力获得方法

2.1 最小水平主应力

在水力压裂过程中,裂缝沿垂直于最小水平主应力方向扩展,当压裂停止后,裂缝在最小水平主应力的作用下逐渐闭合,裂缝中流体压力最终趋于地层最小水平主应力。因此,水平最小主应力可利用下式计算(Schmitt et al.,1989):

$$\sigma_h = p_c \quad (1)$$

式中, σ_h 为最小水平主应力, MPa; p_c 为闭合压力, MPa。

闭合压力 p_c 依据水力压裂施工压降数据获得。图 2a 为研究区 Z1 井压裂施工停泵后的压降曲线,井底流体压力与压降时间 t 满足负幂指数关系。将图 2a 中测试时间平方根与井底流压绘制曲线,该曲线两段近似线性段交汇点所对应的井底流压即为裂缝闭合压力 p_c (图 2b)。

2.2 最大水平主应力

根据摩尔破裂准则,当岩石破裂为拉伸破裂时,最大水平主应力计算公式为(孟召平等,2010):

$$\sigma_H = 3\sigma_h - p_f + T - p_0 \quad (2)$$

式中: σ_H 为最大水平主应力, MPa; p_f 为破裂压力, MPa, 可以在压裂施工曲线上直接读取; T 为抗

拉强度, MPa; p_0 为孔隙压力, MPa, 相当于原始储层压力。煤层抗拉强度差异较小且数值较小, 对最大水平主应力影响较小, 本文取研究区平均值 0.6 MPa 进行计算。同时, 研究区煤层气井试井得到的原始储层压力与埋深满足线性关系(图 3)。

垂直主应力根据上覆岩柱造成的静重力计算(孙良忠等,2017):

$$\sigma_v = \rho g H \quad (3)$$

式中, σ_v 为垂直主应力, MPa; ρ 为上覆岩石平均密度, kg/m³, 研究区煤层以上地层测井解释平均岩石密度为 2550 kg/m³; g 为重力加速度, m/s², 按 9.8 m/s² 计算。

3 地应力状态

3.1 地应力大小

研究区地应力场最小水平主应力为 8.21~31.39 MPa, 平均 15.78 MPa; 最大水平主应力为 9.82~57.87 MPa, 平均 25.92 MPa; 垂向应力为 17.94~29.92 MPa, 平均 24.91 MPa。整体上看, 研究区平均水平主应力远小于垂直主应力, 整体处于拉张状态(孟召平等,2013)。如图 4a 所示, 最小、最大水平主应力和垂向应力均随着埋深的增大而增大, 但最小、最大水平主应力数据点较为分散。这与牛琳琳等(2018)对鄂尔多斯盆地南缘的研究结果一致。

从埋深 730 m 开始, 以 30 m 为间隔, 分别对埋深和最小、最大水平主应力取平均值, 然后进行线性回归。如图 4b 所示, 最小、最大水平主应力与埋

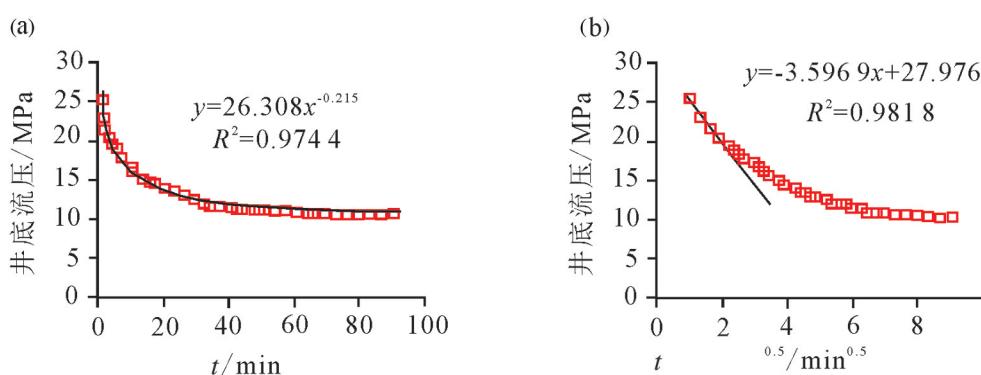


图 2 井底压力与压降时间关系
a—压裂施工压降曲线;b—闭合压力点判识曲线
Fig.2 Relationship between bottom-hole-pressure and the time of pressure drop
a—Pressure drop curve of hydraulic fracturing ;b—Judging curve of closed pressure point

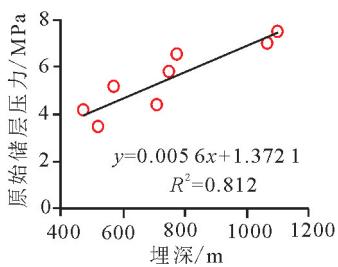


图3 埋深与原始储层压力关系

Fig.3 Relationship between buried depth and the original reservoir pressure

深呈正相关线性关系,则研究区最小、最大水平主应力近似预测公式:

$$\sigma_h = 0.023H - 6.848 \quad (4)$$

$$\sigma_H = 0.043H - 17.394 \quad (5)$$

侧压系数 λ 可以表征不同埋深条件下煤层地应力状态,用下式进行计算(王丹等,2015),

$$\lambda = \frac{\sigma_H + \sigma_h}{2\sigma_v} \quad (6)$$

根据式(6)得到研究区侧压系数,分布在0.42~1.58,平均为0.83;侧压系数随着埋深增加而增加,埋深小于1100 m时,垂向应力最大,煤层处于拉张应力区;埋深大于1100 m后,煤层逐步向挤压型应力状态转变(图5)。

3.2 地应力类型

根据最大、最小水平主应力和垂向应力可以将储层地应力类型划分为3种状态(孙良忠等,2017)。如图6所示,当 $\sigma_v > \sigma_H > \sigma_h$ 时,为Ia型地应力,该类储层容易形成垂直裂缝(孙健等,2017;陈同刚

等,2018;贾慧敏等,2019);当 $\sigma_H > \sigma_h > \sigma_v$ 时,为II型地应力,水平最大主应力为最大应力,垂向应力为最小应力,该类储层容易形成水平裂缝(陈同刚等,2018);当 $\sigma_H > \sigma_v > \sigma_h$ 时,为III型地应力,垂向应力为中间应力,该类储层形成走滑裂缝(陈朝伟等,2014;陈世达等,2018;文卓等,2019;李兵等,2019)。

根据该类型划分标准,研究区地应力类型分布如图7所示,图中灰色区域为Ia类地应力,该区域埋深进一步增大,平均大于990 m,导致其垂向应力最大;白色区域为II类地应力,该区域褶皱发育,表明水平应力较大,最大水平主应力达到33 MPa以上;黑色区域为III类地应力,主要分布在东北部区域。图7表明,该区域地应力类型以Ia类为主,III类其次,II类最少,因此天然裂缝以垂直裂缝为主,以走滑裂缝为辅,水平裂缝较少。

4 对渗透率的影响

4.1 对裂缝发育程度的影响

储层渗透率主要取决于裂缝宽度和密度。采用不同地应力类型条件下煤层气井煤样开展裂缝发育程度扫描电镜实验,定量观测煤样裂缝发育情况,结果如表1所示。表1表明,Ia类地应力类型储层主、次裂缝宽度均最小,分别为8 μm和7 μm;II类地应力类型储层主、次裂缝宽度均最大,分别为16 μm和11 μm;III类储层主、次裂缝宽度居中。从裂缝高度来看,Ia类储层主、次裂缝高度均最大,平均值分别为0.66 cm和0.45 cm;II类储层主、次裂缝高度最小,分别为0.39 cm和0.36 cm,这表明Ia类地

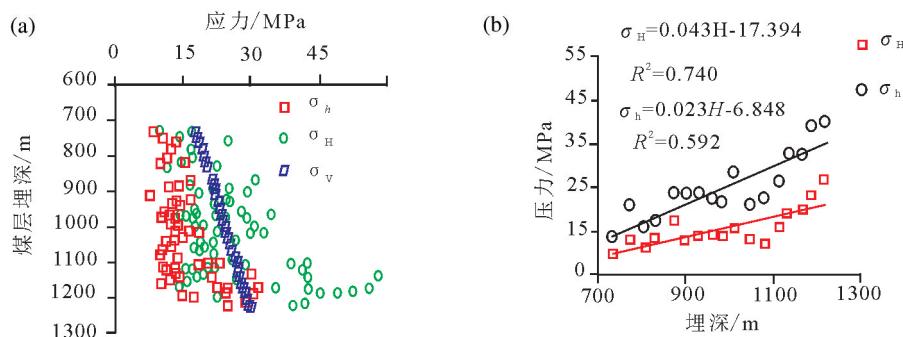


图4 各应力随埋深变化情况

a—全部值;b—平均值

Fig.4 Stress variation with the buried depth

a—All values;b—Mean values

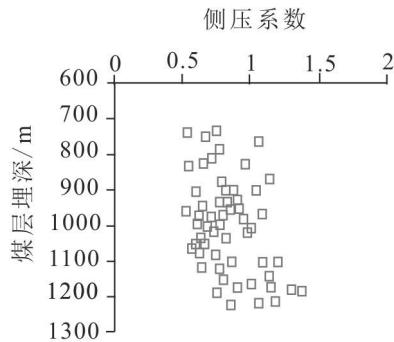


图5 侧压系数随埋深变化情况

Fig.5 Lateral pressure coefficient variation with the buried depth

应力类型更容易发育垂直裂缝。

裂缝渗透率可以用下式表示(贾慧敏等,2017):

$$K_f = \frac{b^3 L}{12A} \quad (7)$$

式中, K_f 为裂缝渗透率, b 为裂缝宽度, L 为渗流面积 A 上的裂缝长度。其中 L/A 可以用裂缝密度来代替,则裂缝渗透率可以近似地用裂缝指数来代替:

$$I_f = b^3 D \quad (8)$$

式中, I_f 为裂缝指数, D 为单位长度上的裂缝密度。利用式(8)对表1中的数据进行计算,得到不同地应力类型储层裂缝指数如表1所示。结果表明,Ia类地应力储层裂缝指数最低,平均为3891.1;II类地应力储层裂缝指数最高,为30739.8,比Ia类地应力储层裂缝指数增大一个数量级;III类地应力储层居中,为7311.2。表明Ia类地应力类型储层渗透性最差,II类地应力类型储层渗透率最好。

4.2 对裂隙应力敏感性影响

在同一块煤样加工成3块规则的正方形煤块,采用三轴加压设备模拟不同地应力类型,然后采用气体测定不同地应力类型条件下有效应力与渗透率关系,如图8所示。部分学者研究表明,煤样有效应力与渗透率关系可以用幂指数关系表示(薛培等,2016;贾慧敏等,2017):

$$k = k_0 \sigma^{-a} \quad (9)$$

式中, k 为有效渗透率; k_0 为初始渗透率; σ 为有效应力; a 为应力敏感性因子,表征应力敏感性强弱,数值越大应力敏感性越强。利用式(9)对图8中测试数据进行回归,结果如图8所示。结果表明,三块煤样初始渗透率相差不大,但Ia类地应力储层应力敏感性系数最小,为0.479,表明该应力状态下,应力敏感性最弱;II类地应力储层应力敏感性系数最大,为0.698,表明应力敏感性最强;III类地应力储层应力敏感性居中。这主要是由于Ia类储层以垂直缝为主,上覆有效应力增加导致的裂缝闭合程度最小,而以水平裂缝为主的II类地应力储层裂缝闭合程度最强。

5 对储层压裂效果的影响

不同地应力类型对储层水力压裂裂缝形态及产量影响,其中裂缝形态和半长通过四维向量微地震监测得到,结果如表2所示。对于Ia类地应力储层,形成垂直缝,导致压裂缝长相对较短,仅为80~100 m;对于II类地应力储层,形成水平缝,裂缝延伸较长,达到130~150 m;对于第III类储层形成复杂缝,裂缝长度居中,主要分布在100~130 m。因此,

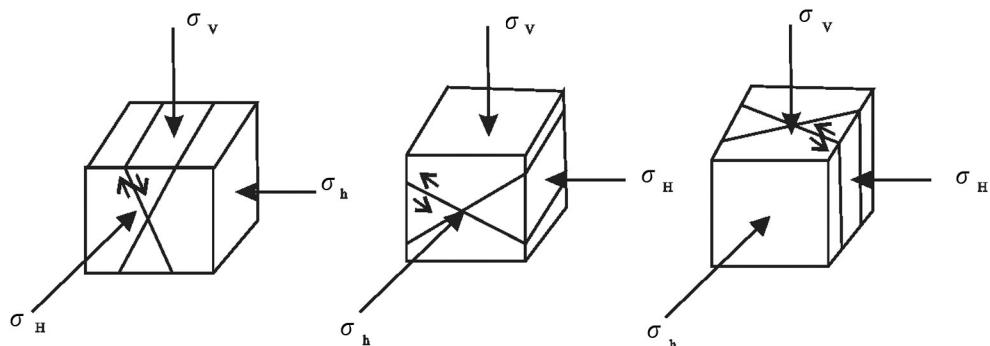


图6 研究区地应力类型示意图(据自孙良忠等,2017修改)

Fig.6 Sketch showing in-situ stress field types(modified from Sun Liangzhong et al., 2017)

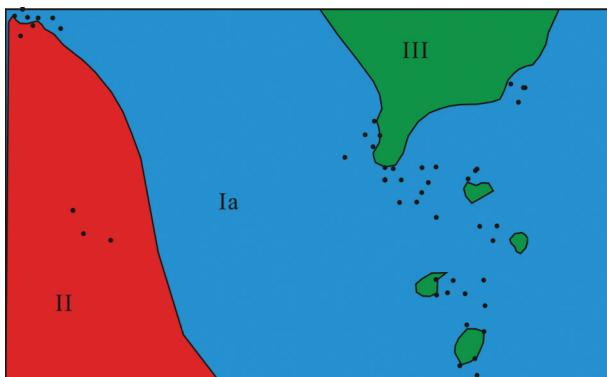


图7 研究区地应力类型分布

Fig.7 Distribution of the in-situ stress field types of South Yanchuan Block

从裂缝形态来看,II类地应力储层压裂效果较好。对研究区域内处于不同地应力类型的压裂煤层气井的累产气量和累产水量进行分析结果表明,处于Ia类地应力状态的井累产水量达到 6800 m^3 ,远高于

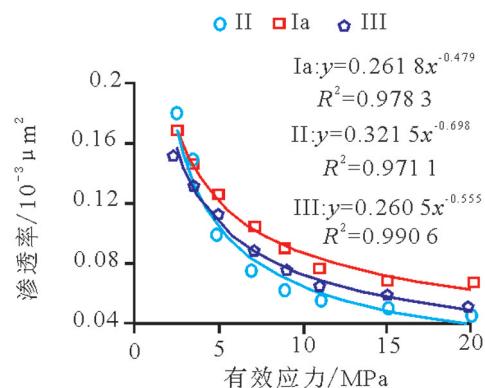


图8 不同地应力类型对煤样应力敏感性影响

Fig.8 Effect of in-situ stress field types on the sensitivity of different coal samples

II类地应力状态的井累产水量 1100 m^3 ,这充分说明Ia类地应力储层形成了垂直裂缝,沟通了上下含水层,导致累产水量增多,II类地应力储层由于为水平缝所以未沟通含水层,故产水量较少;另外处于II类

表1 不同地应力类型对裂缝发育程度的影响

Table 1 Effect of in-situ stress field types on the development degree of fractures

地应力类型	主裂缝			次裂缝			裂缝指数
	高度/cm	宽度/μm	密度/(条·cm ⁻¹)	高度/cm	宽度/μm	密度/(条·cm ⁻¹)	
Ia	0.78	8	7.4	0.47	7	1.8	4406.2
Ia	0.62	9	4.7	0.57	6	2.4	3944.7
Ia	0.72	8	8.3	0.45	8	1.3	4915.2
Ia	0.52	7	3.4	0.3	7	3.3	2298.1
II	0.39	16	6.4	0.36	11	3.4	30739.8
III	0.54	10	6.3	0.38	6	1.9	6710.4
III	0.49	11	4.5	0.18	6	8.9	7911.9

表2 不同地应力类型对压裂缝的影响

Table 2 Effect of in-situ stress field types on the hydraulic fractures

地应力类型	压裂缝形 态	裂缝形态监测结果	压裂缝长 /m	累产水 量/m ³	累产气量 /10 ⁴ m ³
Ia	垂直缝		80~100	6800	16.8
II	水平缝		130~150	1100	91.1
III	复杂裂缝		100~130	4900	18.7

地应力状态的井累产气量达到 $91.1 \times 10^4 \text{ m}^3$,远高于Ia类地应力状态的井累产气量 $16.8 \times 10^4 \text{ m}^3$,这充分说明II类地应力储层形成了较长的压裂裂缝,储层改造效果较好。因此II类地应力储层形成水平缝、压裂缝最长,改造效果最好,产量最高;Ia类地应力储层压形成垂直缝、压裂缝最短,改造效果最差,产量最低,产水量最高;III类地应力储层形成复杂裂缝,缝长居中,但产量相对较低,不能实现效益开发。

6 结 论

(1)研究区各应力值较大,整体处于挤压状态,最小水平主应力为 $8.21\sim31.39 \text{ MPa}$,平均为 15.78 MPa ;最大水平主应力为 $9.82\sim57.87 \text{ MPa}$,平均为 25.92 MPa ;垂向应力为 $17.94\sim29.92 \text{ MPa}$,平均为 24.91 MPa 。最小、最大水平主应力和垂向应力与埋深呈正相关线性关系,最小水平主应力公式为 $\sigma_h = 0.023H - 6.848$,最大水平主应力公式为 $\sigma_H = 0.043H - 17.394$ 。

(2)研究区地应力类型以Ia类为主,III类其次,II类最少。Ia类地应力储层天然裂缝高度最高,以垂直裂缝为主,裂缝指数最低,渗透性最差,但应力敏感性最弱,应力敏感性系数最低为0.479;II类地应力储层主、次裂缝宽度均最大,分别为 $16 \mu\text{m}$ 和 $11 \mu\text{m}$,以水平裂缝为主,裂缝指数最高,达到30739.8,渗透性最高,同时应力敏感性最强;III类地应力储层裂缝复杂,渗透性和应力敏感性居中。

(3)II类地应力储层压裂形成水平缝、压裂缝最长,改造效果最好,产量最高;Ia类地应力储层压裂形成垂直缝、压裂缝最短,改造效果最差,产量最低,产水量最高;III类地应力储层压裂形成复杂裂缝,缝长居中,但产量相对较低,不能实现效益开发。

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